## Attachment 3 <br> to <br> Item 3.1.1

## Transport Assessment

Date of meeting: 17 August 2023
Location: By audio-visual link
Time: 10:00 a.m.

# 172 Commercial Road, Vineyard Transport Assessment 

Prepared for:
EG Funds Management

## PROJECT INFORMATION

| Project Name: | 172 Commercial Road, Vineyard |
| :--- | :--- |
| Client: | EG Funds Management |
| Project Number: | 2325 |
| Prepared By: | JMT Consulting |

## DOCUMENT HISTORY

| Document Title | Revision | Date issued | Author |
| :--- | :--- | :--- | :--- |
| 172 Commercial Road Transport <br> Assessment | Draft | 11.05 .23 | JM |
| 172 Commercial Road Transport <br> Assessment | Draft \#2 | 19.05 .23 | JM |
| 172 Commercial Road Transport <br> Assessment | Issue | 26.05 .23 | JM |

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## 1 Introduction

### 1.1 Background

This Transport Assessment has been prepared by JMT Consulting on behalf of EG Funds Management (EG) to support a Planning Proposal for the site at 172 Commercial Road, Vineyard. The proposal seeks to enable additional permitted uses on the site to enable light industry, warehouses and depot which will in turn permit upgrades/improvements and enhance the environmental management of the site. Potential improvements (subject to a separate detailed DA) may include the following:

- Upgrade of unsealed driveway / hardstand storage areas to sealed surfaces
- Formalisation of the entry, exit and accessways.
- Site-wide landscaping including vegetative buffers to adjoining properties
- Provision of warehouse structures to contain external activity and storage of machinery, equipment and materials


### 1.2 Site location

The site is approximately 4.2 hectares and has direct frontage to two roads Commercial and Chapman Roads. Vineyard train station is located approximately 1.5 km (less than a 5 minute drive) away from the site.


Figure 1 Site location

## 2 Existing Transport Conditions

### 2.1 Road hierarchy

To manage the extensive network of roads for which councils are responsible under the Roads Act 1993, Transport for NSW (TfNSW) in partnership with local government established an administrative framework of State, Regional, and Local Road categories. State Roads are managed and financed by TfNSW and Regional and Local Roads are managed and financed by councils.

Key State and Regional roads which provide access to the site are illustrated in Figure 2 below. Windsor Road to the west of the site is a State Road which provides the primary access route to/from the area - facilitating access to nearby centres including Windsor and Rouse Hill. Bandon Road meets Windsor Road at the intersection with Chapman Road and is a Regional Road that provides connectivity to Vineyard train station. Chapman Road and Commercial Road are local roads under the control of Council.


Figure 2 Surrounding road network

### 2.2 Site access arrangements

Site access arrangements for vehicles are presented in Figure 3 below. Two driveways are currently provided from Chapman Road, with no direct vehicle access currently available from Commercial Road. It should be noted however that access from Commercial Road into the site was previously available however this driveway is gated off and not currently in use.

The southern driveway facilitates the entry of heavy vehicles into the site, with the northern driveway providing for exit movements back onto Chapman Road.


Figure 3
Current site access arrangements

### 2.3 Existing site uses

There are long standing established uses on-site being depot and light industry totalling approximately $3,730 \mathrm{~m}^{2}$ GFA.

## 3 Transport Impact Assessment

### 3.1 Potential site access

The reference scheme prepared for the purposes of the Planning Proposal envisages a rationalisation of vehicle site access as illustrated in Figure 4. The revised site access arrangements include a re-establishing the access point from Commercial Road and connecting this through to the existing southern driveway on Chapman Road through an internal loop road. The existing Chapman Road northern driveway would be closed off under this concept.

The final access arrangements, including details of new/modified driveway crossovers, will be detailed as part of a future Development Application for the site.


Figure 4 Indicative development plan

### 3.2 Car parking

The Hawkesbury Council Development Control Plan (DCP) requires parking for industrial uses to be provided at the following rate:

4 spaces for all development up to $300 m^{2}$ of GFA, then 1 space for each $90 m^{2}$ of GFA or part thereof, in excess of $300 m^{2}$.

Based on the net increase of $5,500 \mathrm{~m}^{2}$ GFA as a result of the proposal (as contemplated under the reference scheme) approximately 62 additional on-site car parking spaces would be required. The quantum and layout of on-site car parking will be detailed as part of a future Development Application for the site.

### 3.3 Forecast traffic generation

The forecast traffic generation arising from the proposal has been determined using trip generation rates outlined in the Transport for NSW Guide to Traffic Generating Developments (TDT 2013/04a) for business parks and industrial estates.

Based on the increase of the additional $5,500 \mathrm{~m}^{2}$ of floor space for the site contemplated under the reference scheme there are expected to be an additional 29 vehicles generated in the morning peak hour and 31 vehicles in the afternoon peak hour as summarised in Table 1. This level of traffic generation is equivalent to approximately one vehicle every two minutes and would not have a significant impact on the surrounding road network.

Table 1 Forecast traffic generation

| Peak Hour | Increase in GFA <br> compared to <br> existing | Traffic <br> generation rate | Vehicles <br> into site | Vehicles <br> out of site | Total <br> vehicles |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AM peak hour |  | 0.52 trips $/ 100 \mathrm{~m}^{2}$ | 20 | 9 | 29 |
|  | $5,500 \mathrm{~m}^{2}$ | 0.56 trips $/ 100 \mathrm{~m}^{2}$ | 9 | 22 | 31 |
|  |  |  |  |  |  |

### 3.4 Road network impacts

### 3.4.1 Overview

Traffic modelling has been undertaken using the TfNSW approved SIDRA modelling software package to consider the impacts of a potential redevelopment of the site at the following intersections:

- Windsor Road / Chapman Road; and
- Chapman Road / Commercial Road.

The traffic modelling metric used to analyse the performance of the road network is Level of Service (LOS). Level of Service is a measure that uses the average delay experienced by vehicles to categorically assign each approach and movement with a qualitative ordinal grade (A through $F$, with $A$ being the best and $F$ being the worst). RMS Traffic Modelling Guidelines indicate the average delay relating to each grade, this is outlined in Table 2. In typical urban environments it is typical for intersections to operate at Level of Service D or E and still remain within acceptable performance levels.

Table 2 Level of service grades / description

| Level of <br> service grade | Average delay <br> (seconds) | Description |
| :---: | :--- | :--- |
| A | Less than 14 | Good operation |
| B to 28 | Good with acceptable delays and spare capacity |  |
| C | 29 to 42 | Satisfactory |
| D | 43 to 56 | Operating near capacity |
| E | 57 to 70 | At capacity. At signals, incidents will cause excessive <br> delays. Roundabouts require other control mode |
| F | Greater than 71 | Unsatisfactory with excessive queuing |

Another common measure of intersection performance is the degree of saturation (DOS), which provides an overall measure of the capability of the intersection to accommodate additional traffic. A DOS of 1.0 indicates that an intersection is operating at capacity.

### 3.4.2 Scenarios considered

The traffic modelling has considered the following two scenarios:
(i) Existing conditions - Based on traffic counts undertaken in March 2023
(ii) Existing conditions + background growth ('Future Base'): A background traffic growth rate of $2.5 \%$ per annum over a 10 year period has been applied. A review of historical traffic data on Windsor Road via the TfNSW traffic volume viewer (station ID 71024) indicates that traffic growth averaged approximately $1.8 \%$ per annum between 2011 and 2019 (i.e. pre COVID years). The $2.5 \%$ assumption is therefore considered robust.
(iii) Existing conditions + background growth + proposal: As per scenario (ii) above with the additional traffic volumes from the Planning Proposal included.

### 3.4.3 Traffic distribution

Based on current traffic flows the majority of traffic is expected to be arrive to the site from Windsor Road given it's status as a classified State Road. The majority of traffic would access the site via the Windsor Road / Chapman Road signalised intersection as indicated in Figure 5 below and travel towards the Chapman Road / Commercial Road intersection. A small proportion of traffic is projected to access the site via Commercial Road.


Figure 5
Forecast traffic distribution

### 3.4.4 Traffic modelling results

The forecast performance of the key intersections surrounding the site is summarised in Table 3 (for the AM peak hour) and Table 4 (for the PM peak hour), with detailed traffic modelling outputs provided as Appendix $A$ of this document.

Table 3 Road network performance - AM Peak Hour (8am - 9am)

| Intersection | Existing Conditions |  | Existing + background <br> growth | Existing + background <br> growth + Proposal |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Degree of <br> Saturation | Level of <br> Service* | Degree of <br> Saturation | Level of <br> Service* | Degree of <br> Saturation | Level of <br> Service* |
| Windsor Road/ <br> Chapman Road | 0.79 | B | 0.94 | C | 0.96 | C |
| Commercial Road <br> /Chapman Road | 0.08 | A | 0.10 | A | 0.11 | A |

Table 4 Road network performance - PM Peak Hour (5pm - 6pm)

| Intersection | Existing Conditions |  | Existing + background <br> growth |  | Existing + background <br> growth + Proposal |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Degree of <br> Saturation | Level of <br> Service $^{*}$ | Degree of <br> Saturation | Level of <br> Service $^{*}$ | Degree of <br> Saturation | Level of <br> Service* |
| Windsor Road / <br> Chapman Road | 0.87 | B | 0.99 | E | 0.99 | E |
| Commercial Road <br> /Chapman Road | 0.09 | A | 0.11 | A | 0.12 | A |

The traffic modelling demonstrates that the relatively small increase in traffic flows associated with a potential redevelopment of the site will not result in adverse impacts on the surrounding road network. The two key intersections in the vicinity of the site retain their Level of Service when compared to a 'future base' scenario. This demonstrates that the proposal can be supported by the existing road network with no additional measures required to accommodate future traffic demands.

### 3.5 Sensitivity analysis

Given the reference scheme represents an indicative design prepared for the purposes of the Planning Proposal, which is subject to change during the development of a detailed Development Application for the site, a sensitivity analysis for the road network has been undertaken which considers both a 'low case' and 'high case' development scenario. These scenarios conducted for the sensitivity analysis are as follows:

- Low case: Additional $3,000 \mathrm{~m}^{2}$ GFA on the site (reduction of $2,500 \mathrm{~m}^{2}$ compared to reference scheme)
- High case: Additional $8,250 \mathrm{~m}^{2}$ GFA on the site (increase of $2,750 \mathrm{~m}^{2}$ compared to reference scheme)

The resultant traffic generation from these scenarios is presented in the tables below.

Table 5 Forecast traffic generation (sensitivity analysis - low case)

| Peak Hour | Increase in GFA <br> compared to <br> existing | Traffic <br> generation rate | Vehicles <br> into site | Vehicles <br> out of site | Total <br> vehicles |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AM peak hour |  | 0.52 trips $/ 100 \mathrm{~m}^{2}$ | 11 | 5 | 16 |
|  | $3,000 \mathrm{~m}^{2}$ | 0.56 trips $/ 100 \mathrm{~m}^{2}$ | 12 | 5 | 17 |
|  |  |  |  |  |  |

Table 6 Forecast traffic generation (sensitivity analysis - high case)

| Peak Hour | Increase in GFA <br> compared to <br> existing | Traffic <br> generation rate | Vehicles <br> into site | Vehicles <br> out of site | Total <br> vehicles |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AM peak hour |  | 0.52 trips $/ 100 \mathrm{~m}^{2}$ | 30 | 13 | 43 |
|  | $8,250 \mathrm{~m}^{2}$ | 0.56 trips $/ 100 \mathrm{~m}^{2}$ | 32 | 14 | 46 |
| PM peak hour |  |  |  | 43 |  |

Table 7 Road network performance - sensitivity test - AM Peak Hour

| Intersection | Low Case <br> (Additional 3,000m²) |  | Base Case <br> (Additional 5,500m²) |  | High Case <br> (Additional 8,250m²) |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Degree of <br> Saturation | Level of <br> Service | Degree of <br> Saturation | Level of <br> Service* | Degree of <br> Saturation | Level of <br> Service |
| Windsor Road / <br> Chapman Road | 0.94 | C | 0.96 | C | 0.95 | C |
| Commercial Road <br> /Chapman Road | 0.10 | A | 0.11 | A | 0.11 | A |

Table 8 Road network performance - sensitivity test - PM Peak Hour

| Intersection | Low Case <br> (Additional 3,000m²) |  | Base Case <br> (Additional 5,500m²) |  | High Case <br> (Additional 8,250m²) |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Degree of <br> Saturation | Level of <br> Service* | Degree of <br> Saturation | Level of <br> Service* | Degree of <br> Saturation | Level of <br> Service* |
| Windsor Road / <br> Chapman Road | 0.99 | E | 0.99 | E | 0.99 | E |
| Commercial Road <br> / Chapman Road | 0.11 | A | 0.12 | A | 0.12 | A |

The sensitivity analysis demonstrates that the nearby intersections will operate in a very similar manner under the range of scenarios considered. The level of service remains unchanged under both the 'low' and 'high' scenarios in comparison to the reference scheme - demonstrating the volume of additional traffic generated by any future development of the site would be negligible in the context of background traffic flows.

This sensitivity analysis provides further confidence that any future development arising from the Planning Proposal will not unduly impact the performance of the surrounding road network.

## 4 Summary

JMT Consulting has prepared this transport impact assessment to support a Planning Proposal for the site at 172 Commercial Road, Vineyard. The proposal seeks to enable additional permitted uses on the site to enable light industry, warehouses and depot which will in turn permit upgrades/improvements and enhance the environmental management of the site.

The reference scheme developed for the proposal envisages a rationalisation of vehicle site access compared to current conditions - providing an overall benefit for the surrounding road network. Details around vehicle site access locations and car parking numbers would be outlined as part of a future Development Application for the site.

The proposal may result in additional traffic movements of approximately 30 vehicles per hour in the commuter peak periods - equivalent to one vehicle every two minutes. This level of traffic generation is equivalent to approximately one vehicle every two minutes and would not have a significant impact on the surrounding road network.

Traffic modelling undertaken in accordance with Transport for NSW guidelines demonstrates that the operation of key intersections in the vicinity of the site will not be impacted by the small number of additional vehicle movements associated with a future DA for the site. A sensitivity assessment was conducted which considered both a low and high case development scenario. This sensitivity assessment showed the level of service of key intersections remained unchanged under the scenarios modelled - confirming that any future development arising from the Planning Proposal will not unduly impact the performance of the surrounding road network.

In the above context the traffic and transport impacts of the Planning Proposal are considered acceptable.

## Appendix A: Traffic Modelling Outputs

## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [AM Existing (Site Folder: General)]

New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | MES <br> HV ] <br> \% |  | AND NS HV ] \% | Deg. Satn v/c | Aver. Delay sec | Level of Service | 95\% <br> [ Veh veh | CK OF Dist ] | Prop. Que | Effective Stop Rate | Aver No. Cycles | Aver. Speed km/h |
| South: Chapman Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 67 | 7.5 | 71 | 7.5 | 0.045 | 5.7 | LOSA | 0.2 | 1.4 | 0.07 | 0.55 | 0.07 | 53.1 |
| 2 T1 | 28 | 10.7 | 29 | 10.7 | 0.059 | 4.8 | LOS A | 0.2 | 1.6 | 0.27 | 0.57 | 0.27 | 53.3 |
| 3 R2 | 24 | 25.0 | 25 | 25.0 | 0.059 | 7.1 | LOS A | 0.2 | 1.6 | 0.27 | 0.57 | 0.27 | 51.9 |
| Approach | 119 | 11.8 | 125 | 11.8 | 0.059 | 5.8 | LOS A | 0.2 | 1.6 | 0.16 | 0.56 | 0.16 | 52.9 |
| East: Commerial Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 18 | 11.1 | 19 | 11.1 | 0.023 | 5.7 | LOS A | 0.0 | 0.3 | 0.01 | 0.35 | 0.01 | 54.9 |
| 5 T1 | 15 | 13.3 | 16 | 13.3 | 0.023 | 0.0 | LOSA | 0.0 | 0.3 | 0.01 | 0.35 | 0.01 | 56.9 |
| 6 R2 | 4 | 25.0 | 4 | 25.0 | 0.023 | 5.8 | LOSA | 0.0 | 0.3 | 0.01 | 0.35 | 0.01 | 53.7 |
| Approach | 37 | 13.5 | 39 | 13.5 | 0.023 | 3.4 | NA | 0.0 | 0.3 | 0.01 | 0.35 | 0.01 | 55.5 |
| North: Bocks Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 1 | 0.0 | 1 | 0.0 | 0.065 | 5.6 | LOS A | 0.2 | 1.7 | 0.18 | 0.53 | 0.18 | 54.2 |
| 8 T1 | 65 | 4.6 | 68 | 4.6 | 0.065 | 4.8 | LOS A | 0.2 | 1.7 | 0.18 | 0.53 | 0.18 | 54.1 |
| 9 R2 | 3 | 33.3 | 3 | 33.3 | 0.065 | 7.5 | LOS A | 0.2 | 1.7 | 0.18 | 0.53 | 0.18 | 52.1 |
| Approach | 69 | 5.8 | 73 | 5.8 | 0.065 | 4.9 | LOS A | 0.2 | 1.7 | 0.18 | 0.53 | 0.18 | 54.1 |
| West: Commerial Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 2 | 0.0 | 2 | 0.0 | 0.078 | 5.7 | LOS A | 0.3 | 2.4 | 0.12 | 0.53 | 0.12 | 53.5 |
| 11 T1 | 4 | 0.0 | 4 | 0.0 | 0.078 | 0.1 | LOS A | 0.3 | 2.4 | 0.12 | 0.53 | 0.12 | 54.8 |
| 12 R 2 | 96 | 4.2 | 101 | 4.2 | 0.078 | 5.7 | LOS A | 0.3 | 2.4 | 0.12 | 0.53 | 0.12 | 53.0 |
| Approach | 102 | 3.9 | 107 | 3.9 | 0.078 | 5.5 | NA | 0.3 | 2.4 | 0.12 | 0.53 | 0.12 | 53.1 |
| All Vehicles | 327 | 8.3 | 344 | 8.3 | 0.078 | 5.2 | NA | 0.3 | 2.4 | 0.13 | 0.52 | 0.13 | 53.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [AM Existing + Background Growth (Site Folder:
General)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLu } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { VES } \\ & \text { HV ] } \\ & \% \\ & \hline \end{aligned}$ |  | $\begin{gathered} \text { HD } \\ \text { NS } \\ \text { HV] } \\ \% \\ \hline \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \\ \hline \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Chapman Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 87 | 11.5 | 92 | 11.5 | 0.060 | 5.7 | LOS A | 0.2 | 1.9 | 0.08 | 0.55 | 0.08 | 52.9 |
| 2 T1 | 36 | 16.7 | 38 | 16.7 | 0.080 | 5.2 | LOS A | 0.3 | 2.4 | 0.32 | 0.59 | 0.32 | 52.8 |
| 3 R2 | 28 | 35.7 | 29 | 35.7 | 0.080 | 7.9 | LOS A | 0.3 | 2.4 | 0.32 | 0.59 | 0.32 | 51.1 |
| Approach | 151 | 17.2 | 159 | 17.2 | 0.080 | 6.0 | LOS A | 0.3 | 2.4 | 0.19 | 0.57 | 0.19 | 52.5 |
| East: Commerial Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 24 | 16.7 | 25 | 16.7 | 0.033 | 5.7 | LOSA | 0.1 | 0.5 | 0.02 | 0.35 | 0.02 | 54.6 |
| 5 T1 | 20 | 20.0 | 21 | 20.0 | 0.033 | 0.0 | LOSA | 0.1 | 0.5 | 0.02 | 0.35 | 0.02 | 56.8 |
| 6 R2 | 6 | 33.3 | 6 | 33.3 | 0.033 | 5.9 | LOS A | 0.1 | 0.5 | 0.02 | 0.35 | 0.02 | 53.2 |
| Approach | 50 | 20.0 | 53 | 20.0 | 0.033 | 3.5 | NA | 0.1 | 0.5 | 0.02 | 0.35 | 0.02 | 55.3 |
| North: Bocks Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 2 | 0.0 | 2 | 0.0 | 0.094 | 5.6 | LOS A | 0.3 | 2.6 | 0.20 | 0.55 | 0.20 | 53.9 |
| 8 T1 | 85 | 8.2 | 89 | 8.2 | 0.094 | 5.1 | LOS A | 0.3 | 2.6 | 0.20 | 0.55 | 0.20 | 53.8 |
| 9 R2 | 5 | 40.0 | 5 | 40.0 | 0.094 | 8.4 | LOSA | 0.3 | 2.6 | 0.20 | 0.55 | 0.20 | 51.6 |
| Approach | 92 | 9.8 | 97 | 9.8 | 0.094 | 5.3 | LOS A | 0.3 | 2.6 | 0.20 | 0.55 | 0.20 | 53.6 |
| West: Commerial Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 3 | 0.0 | 3 | 0.0 | 0.100 | 5.7 | LOS A | 0.4 | 3.2 | 0.14 | 0.53 | 0.14 | 53.4 |
| 11 T1 | 6 | 0.0 | 6 | 0.0 | 0.100 | 0.2 | LOSA | 0.4 | 3.2 | 0.14 | 0.53 | 0.14 | 54.8 |
| 12 R 2 | 120 | 6.7 | 126 | 6.7 | 0.100 | 5.8 | LOSA | 0.4 | 3.2 | 0.14 | 0.53 | 0.14 | 52.9 |
| Approach | 129 | 6.2 | 136 | 6.2 | 0.100 | 5.5 | NA | 0.4 | 3.2 | 0.14 | 0.53 | 0.14 | 53.0 |
| All <br> Vehicles | 422 | 12.6 | 444 | 12.6 | 0.100 | 5.4 | NA | 0.4 | 3.2 | 0.16 | 0.52 | 0.16 | 53.2 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [AM Existing + Background Growth + Proposal (Site
Folder: General)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { IN } \\ \mathrm{VOL} \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{gathered} \text { JT } \\ \text { MES } \\ \text { HV ] } \\ \% \end{gathered}$ |  | $\begin{gathered} \text { AND } \\ \text { WS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \\ \hline \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver Speed <br> km/h |
| South: Chapman Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 105 | 8.8 | 111 | 8.8 | 0.072 | 5.7 | LOS A | 0.3 | 2.3 | 0.09 | 0.55 | 0.09 | 53.0 |
| 2 T1 | 36 | 16.7 | 38 | 16.7 | 0.073 | 5.2 | LOSA | 0.3 | 2.2 | 0.33 | 0.59 | 0.33 | 52.8 |
| 3 R2 | 23 | 35.7 | 24 | 35.7 | 0.073 | 8.0 | LOSA | 0.3 | 2.2 | 0.33 | 0.59 | 0.33 | 51.2 |
| Approach | 164 | 14.3 | 173 | 14.3 | 0.073 | 5.9 | LOS A | 0.3 | 2.3 | 0.17 | 0.56 | 0.17 | 52.7 |
| East: Commerial Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 24 | 16.7 | 25 | 16.7 | 0.034 | 5.7 | LOS A | 0.1 | 0.5 | 0.02 | 0.33 | 0.02 | 54.8 |
| 5 T1 | 22 | 14.8 | 23 | 14.8 | 0.034 | 0.0 | LOSA | 0.1 | 0.5 | 0.02 | 0.33 | 0.02 | 57.0 |
| 6 R2 | 6 | 33.3 | 6 | 33.3 | 0.034 | 5.9 | LOSA | 0.1 | 0.5 | 0.02 | 0.33 | 0.02 | 53.4 |
| Approach | 52 | 17.8 | 55 | 17.8 | 0.034 | 3.3 | NA | 0.1 | 0.5 | 0.02 | 0.33 | 0.02 | 55.5 |
| North: Bocks Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 2 | 0.0 | 2 | 0.0 | 0.095 | 5.6 | LOSA | 0.4 | 2.7 | 0.20 | 0.55 | 0.20 | 53.9 |
| 8 T1 | 85 | 8.2 | 89 | 8.2 | 0.095 | 5.1 | LOS A | 0.4 | 2.7 | 0.20 | 0.55 | 0.20 | 53.7 |
| 9 R2 | 5 | 40.0 | 5 | 40.0 | 0.095 | 8.7 | LOSA | 0.4 | 2.7 | 0.20 | 0.55 | 0.20 | 51.5 |
| Approach | 92 | 9.8 | 97 | 9.8 | 0.095 | 5.3 | LOS A | 0.4 | 2.7 | 0.20 | 0.55 | 0.20 | 53.6 |
| West: Commerial Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 3 | 0.0 | 3 | 0.0 | 0.106 | 5.8 | LOS A | 0.5 | 3.4 | 0.15 | 0.53 | 0.15 | 53.4 |
| 11 T1 | 6 | 0.0 | 6 | 0.0 | 0.106 | 0.2 | LOS A | 0.5 | 3.4 | 0.15 | 0.53 | 0.15 | 54.8 |
| 12 R 2 | 128 | 5.7 | 135 | 5.7 | 0.106 | 5.8 | LOSA | 0.5 | 3.4 | 0.15 | 0.53 | 0.15 | 52.9 |
| Approach | 137 | 5.3 | 144 | 5.3 | 0.106 | 5.5 | NA | 0.5 | 3.4 | 0.15 | 0.53 | 0.15 | 53.0 |
| All <br> Vehicles | 445 | 11.0 | 468 | 11.0 | 0.106 | 5.4 | NA | 0.5 | 3.4 | 0.15 | 0.52 | 0.15 | 53.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [AM Existing + Background Growth + Proposal <br> (Low Case) (Site Folder: General)]

New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { IN } \\ \mathrm{VOL} \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{gathered} \text { JT } \\ \text { MES } \\ \text { HV ] } \\ \% \end{gathered}$ |  | $\begin{gathered} \text { AND } \\ \text { WS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. <br> Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver Speed <br> km/h |
| South: Chapman Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 97 | 8.8 | 102 | 8.8 | 0.066 | 5.7 | LOS A | 0.3 | 2.1 | 0.08 | 0.55 | 0.08 | 53.0 |
| 2 T1 | 36 | 16.7 | 38 | 16.7 | 0.073 | 5.2 | LOS A | 0.3 | 2.2 | 0.32 | 0.59 | 0.32 | 52.9 |
| 3 R2 | 23 | 35.7 | 24 | 35.7 | 0.073 | 7.9 | LOSA | 0.3 | 2.2 | 0.32 | 0.59 | 0.32 | 51.2 |
| Approach | 156 | 14.6 | 164 | 14.6 | 0.073 | 5.9 | LOS A | 0.3 | 2.2 | 0.17 | 0.56 | 0.17 | 52.7 |
| East: Commerial Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 24 | 16.7 | 25 | 16.7 | 0.033 | 5.7 | LOS A | 0.1 | 0.5 | 0.02 | 0.34 | 0.02 | 54.7 |
| 5 T1 | 21 | 14.8 | 22 | 14.8 | 0.033 | 0.0 | LOSA | 0.1 | 0.5 | 0.02 | 0.34 | 0.02 | 57.0 |
| 6 R2 | 6 | 33.3 | 6 | 33.3 | 0.033 | 5.9 | LOSA | 0.1 | 0.5 | 0.02 | 0.34 | 0.02 | 53.3 |
| Approach | 51 | 17.9 | 54 | 17.9 | 0.033 | 3.4 | NA | 0.1 | 0.5 | 0.02 | 0.34 | 0.02 | 55.5 |
| North: Bocks Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 2 | 0.0 | 2 | 0.0 | 0.095 | 5.6 | LOSA | 0.3 | 2.7 | 0.20 | 0.55 | 0.20 | 53.9 |
| 8 T1 | 85 | 8.2 | 89 | 8.2 | 0.095 | 5.1 | LOSA | 0.3 | 2.7 | 0.20 | 0.55 | 0.20 | 53.7 |
| 9 R2 | 5 | 40.0 | 5 | 40.0 | 0.095 | 8.6 | LOSA | 0.3 | 2.7 | 0.20 | 0.55 | 0.20 | 51.6 |
| Approach | 92 | 9.8 | 97 | 9.8 | 0.095 | 5.3 | LOS A | 0.3 | 2.7 | 0.20 | 0.55 | 0.20 | 53.6 |
| West: Commerial Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 3 | 0.0 | 3 | 0.0 | 0.103 | 5.8 | LOS A | 0.4 | 3.2 | 0.15 | 0.53 | 0.15 | 53.4 |
| 11 T1 | 6 | 0.0 | 6 | 0.0 | 0.103 | 0.2 | LOS A | 0.4 | 3.2 | 0.15 | 0.53 | 0.15 | 54.8 |
| 12 R 2 | 124 | 5.7 | 131 | 5.7 | 0.103 | 5.8 | LOSA | 0.4 | 3.2 | 0.15 | 0.53 | 0.15 | 52.9 |
| Approach | 133 | 5.3 | 140 | 5.3 | 0.103 | 5.5 | NA | 0.4 | 3.2 | 0.15 | 0.53 | 0.15 | 53.0 |
| All <br> Vehicles | 432 | 11.1 | 455 | 11.1 | 0.103 | 5.4 | NA | 0.4 | 3.2 | 0.15 | 0.52 | 0.15 | 53.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [AM Existing + Background Growth + Proposal <br> (High Case) (Site Folder: General)]

New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{gathered} \text { HND } \\ \text { NS } \\ \text { HV] } \\ \% \\ \hline \end{gathered}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | CK OF <br> UE Dist ] m | Prop. Que | Effective Stop Rate |  | Aver. Speed <br> km/h |
| South: Chapman Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 114 | 8.8 | 120 | 8.8 | 0.078 | 5.7 | LOS A | 0.3 | 2.5 | 0.09 | 0.55 | 0.09 | 53.0 |
| 2 T1 | 36 | 16.7 | 38 | 16.7 | 0.074 | 5.2 | LOS A | 0.3 | 2.2 | 0.33 | 0.59 | 0.33 | 52.8 |
| 3 R2 | 23 | 35.7 | 24 | 35.7 | 0.074 | 8.0 | LOSA | 0.3 | 2.2 | 0.33 | 0.59 | 0.33 | 51.2 |
| Approach | 173 | 14.0 | 182 | 14.0 | 0.078 | 5.9 | LOS A | 0.3 | 2.5 | 0.17 | 0.56 | 0.17 | 52.7 |
| East: Commerial Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 24 | 16.7 | 25 | 16.7 | 0.034 | 5.7 | LOS A | 0.1 | 0.5 | 0.02 | 0.33 | 0.02 | 54.8 |
| 5 T1 | 23 | 14.8 | 24 | 14.8 | 0.034 | 0.0 | LOSA | 0.1 | 0.5 | 0.02 | 0.33 | 0.02 | 57.1 |
| 6 R2 | 6 | 33.3 | 6 | 33.3 | 0.034 | 5.9 | LOSA | 0.1 | 0.5 | 0.02 | 0.33 | 0.02 | 53.4 |
| Approach | 53 | 17.7 | 56 | 17.7 | 0.034 | 3.3 | NA | 0.1 | 0.5 | 0.02 | 0.33 | 0.02 | 55.6 |
| North: Bocks Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 2 | 0.0 | 2 | 0.0 | 0.096 | 5.6 | LOS A | 0.4 | 2.7 | 0.20 | 0.55 | 0.20 | 53.8 |
| 8 T1 | 85 | 8.2 | 89 | 8.2 | 0.096 | 5.2 | LOSA | 0.4 | 2.7 | 0.20 | 0.55 | 0.20 | 53.7 |
| 9 R2 | 5 | 40.0 | 5 | 40.0 | 0.096 | 8.9 | LOSA | 0.4 | 2.7 | 0.20 | 0.55 | 0.20 | 51.5 |
| Approach | 92 | 9.8 | 97 | 9.8 | 0.096 | 5.4 | LOS A | 0.4 | 2.7 | 0.20 | 0.55 | 0.20 | 53.6 |
| West: Commerial Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 3 | 0.0 | 3 | 0.0 | 0.110 | 5.8 | LOS A | 0.5 | 3.5 | 0.15 | 0.53 | 0.15 | 53.4 |
| 11 T1 | 6 | 0.0 | 6 | 0.0 | 0.110 | 0.2 | LOS A | 0.5 | 3.5 | 0.15 | 0.53 | 0.15 | 54.7 |
| 12 R 2 | 132 | 5.7 | 139 | 5.7 | 0.110 | 5.8 | LOSA | 0.5 | 3.5 | 0.15 | 0.53 | 0.15 | 52.9 |
| Approach | 141 | 5.3 | 148 | 5.3 | 0.110 | 5.6 | NA | 0.5 | 3.5 | 0.15 | 0.53 | 0.15 | 53.0 |
| All <br> Vehicles | 459 | 10.9 | 483 | 10.9 | 0.110 | 5.4 | NA | 0.5 | 3.5 | 0.15 | 0.52 | 0.15 | 53.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

## $\nabla$ Site: 101 [PM Existing (Site Folder: General)]

New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  |  |  | ND NS HV ] \% | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service | 95\% <br> [ Veh. veh | CK OF JE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Chapman Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| L2 | 72 | 9.7 | 76 | 9.7 | 0.049 | 5.7 | LOSA | 0.2 | 1.5 | 0.05 | 0.55 | 0.05 | 53.1 |
| 2 T1 | 53 | 0.0 | 56 | 0.0 | 0.090 | 4.5 | LOS A | 0.3 | 2.4 | 0.21 | 0.55 | 0.21 | 53.9 |
| 3 R2 | 38 | 18.4 | 40 | 18.4 | 0.090 | 6.4 | LOS A | 0.3 | 2.4 | 0.21 | 0.55 | 0.21 | 52.4 |
| Approach | 163 | 8.6 | 172 | 8.6 | 0.090 | 5.5 | LOS A | 0.3 | 2.4 | 0.14 | 0.55 | 0.14 | 53.2 |
| East: Commerial Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 31 | 12.9 | 33 | 12.9 | 0.028 | 5.7 | LOS A | 0.0 | 0.4 | 0.01 | 0.47 | 0.01 | 53.8 |
| 5 T1 | 8 | 12.5 | 8 | 12.5 | 0.028 | 0.0 | LOS A | 0.0 | 0.4 | 0.01 | 0.47 | 0.01 | 55.8 |
| 6 R2 | 5 | 20.0 | 5 | 20.0 | 0.028 | 5.7 | LOSA | 0.0 | 0.4 | 0.01 | 0.47 | 0.01 | 52.9 |
| Approach | 44 | 13.6 | 46 | 13.6 | 0.028 | 4.7 | NA | 0.0 | 0.4 | 0.01 | 0.47 | 0.01 | 54.1 |
| North: Bocks Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 1 | 0.0 | 1 | 0.0 | 0.034 | 5.6 | LOS A | 0.1 | 0.9 | 0.13 | 0.52 | 0.13 | 54.3 |
| 8 T1 | 36 | 5.6 | 38 | 5.6 | 0.034 | 4.6 | LOS A | 0.1 | 0.9 | 0.13 | 0.52 | 0.13 | 54.2 |
| 9 R2 | 1 | 0.0 | 1 | 0.0 | 0.034 | 6.4 | LOS A | 0.1 | 0.9 | 0.13 | 0.52 | 0.13 | 53.7 |
| Approach | 38 | 5.3 | 40 | 5.3 | 0.034 | 4.7 | LOSA | 0.1 | 0.9 | 0.13 | 0.52 | 0.13 | 54.2 |
| West: Commerial Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 3 | 0.0 | 3 | 0.0 | 0.044 | 5.7 | LOS A | 0.2 | 1.3 | 0.12 | 0.51 | 0.12 | 53.6 |
| 11 T1 | 4 | 0.0 | 4 | 0.0 | 0.044 | 0.2 | LOSA | 0.2 | 1.3 | 0.12 | 0.51 | 0.12 | 54.9 |
| 12 R 2 | 52 | 1.9 | 55 | 1.9 | 0.044 | 5.7 | LOS A | 0.2 | 1.3 | 0.12 | 0.51 | 0.12 | 53.2 |
| Approach | 59 | 1.7 | 62 | 1.7 | 0.044 | 5.3 | NA | 0.2 | 1.3 | 0.12 | 0.51 | 0.12 | 53.4 |
| All <br> Vehicles | 304 | 7.6 | 320 | 7.6 | 0.090 | 5.2 | NA | 0.3 | 2.4 | 0.12 | 0.53 | 0.12 | 53.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\nabla$ Site: 101 [PM Existing + Background Growth (Site Folder:
General)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLu } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { VES } \\ & \text { HV ] } \\ & \% \\ & \hline \end{aligned}$ |  | $\begin{gathered} \text { HD } \\ \text { NS } \\ \text { HV] } \\ \% \\ \hline \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \\ \hline \end{gathered}$ | Prop. Que | Effective Stop Rate | $\begin{aligned} & \text { Aver. } \\ & \text { No. } \\ & \text { Cycles } \end{aligned}$ | Aver. Speed <br> km/h |
| South: Chapman Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 88 | 13.6 | 93 | 13.6 | 0.061 | 5.7 | LOS A | 0.3 | 2.0 | 0.06 | 0.55 | 0.06 | 52.8 |
| 2 T1 | 69 | 0.0 | 73 | 0.0 | 0.114 | 4.7 | LOS A | 0.4 | 3.2 | 0.26 | 0.56 | 0.26 | 53.8 |
| 3 R2 | 40 | 30.0 | 42 | 30.0 | 0.114 | 7.1 | LOSA | 0.4 | 3.2 | 0.26 | 0.56 | 0.26 | 51.8 |
| Approach | 197 | 12.2 | 207 | 12.2 | 0.114 | 5.6 | LOS A | 0.4 | 3.2 | 0.17 | 0.55 | 0.17 | 53.0 |
| East: Commerial Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 42 | 16.7 | 44 | 16.7 | 0.041 | 5.7 | LOSA | 0.1 | 0.6 | 0.02 | 0.45 | 0.02 | 53.8 |
| 5 T1 | 13 | 15.4 | 14 | 15.4 | 0.041 | 0.0 | LOSA | 0.1 | 0.6 | 0.02 | 0.45 | 0.02 | 55.9 |
| 6 R2 | 8 | 25.0 | 8 | 25.0 | 0.041 | 5.8 | LOS A | 0.1 | 0.6 | 0.02 | 0.45 | 0.02 | 52.8 |
| Approach | 63 | 17.5 | 66 | 17.5 | 0.041 | 4.6 | NA | 0.1 | 0.6 | 0.02 | 0.45 | 0.02 | 54.1 |
| North: Bocks Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 2 | 0.0 | 2 | 0.0 | 0.052 | 5.6 | LOS A | 0.2 | 1.4 | 0.15 | 0.53 | 0.15 | 54.1 |
| 8 T1 | 51 | 5.9 | 54 | 5.9 | 0.052 | 4.8 | LOSA | 0.2 | 1.4 | 0.15 | 0.53 | 0.15 | 54.1 |
| 9 R2 | 2 | 0.0 | 2 | 0.0 | 0.052 | 6.8 | LOSA | 0.2 | 1.4 | 0.15 | 0.53 | 0.15 | 53.6 |
| Approach | 55 | 5.5 | 58 | 5.5 | 0.052 | 4.9 | LOS A | 0.2 | 1.4 | 0.15 | 0.53 | 0.15 | 54.1 |
| West: Commerial Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 5 | 0.0 | 5 | 0.0 | 0.059 | 5.8 | LOSA | 0.2 | 1.8 | 0.16 | 0.51 | 0.16 | 53.5 |
| 11 T1 | 6 | 0.0 | 6 | 0.0 | 0.059 | 0.2 | LOSA | 0.2 | 1.8 | 0.16 | 0.51 | 0.16 | 54.9 |
| 12 R 2 | 66 | 6.1 | 69 | 6.1 | 0.059 | 5.8 | LOSA | 0.2 | 1.8 | 0.16 | 0.51 | 0.16 | 53.0 |
| Approach | 77 | 5.2 | 81 | 5.2 | 0.059 | 5.4 | NA | 0.2 | 1.8 | 0.16 | 0.51 | 0.16 | 53.2 |
| All <br> Vehicles | 392 | 10.7 | 413 | 10.7 | 0.114 | 5.3 | NA | 0.4 | 3.2 | 0.14 | 0.53 | 0.14 | 53.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [PM Existing + Background Growth + Growth (Site
Folder: General)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{gathered} \text { IN } \\ \text { VOL } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{aligned} & \text { UT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { AND } \\ & \text { WS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{aligned} & 95 \% \text { B } \\ & \text { QU } \\ & \text { [ Veh. } \\ & \text { veh } \end{aligned}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver No. Cycles | Aver. Speed <br> km/h |
| South: Chapman Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 93 | 12.4 | 98 | 12.4 | 0.064 | 5.7 | LOS A | 0.3 | 2.1 | 0.06 | 0.55 | 0.06 | 52.9 |
| 2 T1 | 69 | 0.0 | 73 | 0.0 | 0.117 | 4.7 | LOSA | 0.4 | 3.3 | 0.28 | 0.57 | 0.28 | 53.8 |
| $3 \quad \mathrm{R} 2$ | 40 | 30.0 | 42 | 30.0 | 0.117 | 7.2 | LOSA | 0.4 | 3.3 | 0.28 | 0.57 | 0.28 | 51.7 |
| Approach | 202 | 11.6 | 213 | 11.6 | 0.117 | 5.7 | LOS A | 0.4 | 3.3 | 0.18 | 0.56 | 0.18 | 53.0 |
| East: Commerial Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 42 | 16.7 | 44 | 16.7 | 0.040 | 5.7 | LOS A | 0.1 | 0.6 | 0.02 | 0.47 | 0.02 | 53.6 |
| 5 T1 | 11 | 15.4 | 12 | 15.4 | 0.040 | 0.0 | LOSA | 0.1 | 0.6 | 0.02 | 0.47 | 0.02 | 55.8 |
| 6 R2 | 8 | 25.0 | 8 | 25.0 | 0.040 | 5.8 | LOSA | 0.1 | 0.6 | 0.02 | 0.47 | 0.02 | 52.7 |
| Approach | 61 | 17.5 | 64 | 17.5 | 0.040 | 4.7 | NA | 0.1 | 0.6 | 0.02 | 0.47 | 0.02 | 53.9 |
| North: Bocks Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 2 | 0.0 | 2 | 0.0 | 0.053 | 5.6 | LOS A | 0.2 | 1.4 | 0.16 | 0.53 | 0.16 | 54.1 |
| 8 T1 | 51 | 5.9 | 54 | 5.9 | 0.053 | 4.9 | LOS A | 0.2 | 1.4 | 0.16 | 0.53 | 0.16 | 54.0 |
| 9 R2 | 2 | 0.0 | 2 | 0.0 | 0.053 | 7.0 | LOSA | 0.2 | 1.4 | 0.16 | 0.53 | 0.16 | 53.5 |
| Approach | 55 | 5.5 | 58 | 5.5 | 0.053 | 5.0 | LOS A | 0.2 | 1.4 | 0.16 | 0.53 | 0.16 | 54.0 |
| West: Commerial Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 5 | 0.0 | 5 | 0.0 | 0.075 | 5.8 | LOSA | 0.3 | 2.3 | 0.16 | 0.51 | 0.16 | 53.5 |
| 11 T1 | 7 | 0.0 | 7 | 0.0 | 0.075 | 0.2 | LOSA | 0.3 | 2.3 | 0.16 | 0.51 | 0.16 | 54.9 |
| 12 R 2 | 86 | 4.2 | 91 | 4.2 | 0.075 | 5.8 | LOSA | 0.3 | 2.3 | 0.16 | 0.51 | 0.16 | 53.1 |
| Approach | 98 | 3.7 | 103 | 3.7 | 0.075 | 5.4 | NA | 0.3 | 2.3 | 0.16 | 0.51 | 0.16 | 53.2 |
| All <br> Vehicles | 416 | 9.8 | 438 | 9.8 | 0.117 | 5.4 | NA | 0.4 | 3.3 | 0.15 | 0.53 | 0.15 | 53.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: C:\JMT ConsultinglProjects\2325-172 Commercial Road, Vineyard\Internall172 Commercial Road SIDRA_Commercial Road.sip9

## MOVEMENT SUMMARY

$\nabla$ Site: 101 [PM Existing + Background Growth + Growth (Low
Case) (Site Folder: General)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INP } \\ & \text { VOLu } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { VES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{gathered} \text { HD } \\ \text { NS } \\ \text { HV] } \\ \% \\ \hline \end{gathered}$ | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { UE } \\ \text { Dist ] } \\ \text { m } \\ \hline \end{gathered}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Chapman Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 90 | 12.4 | 95 | 12.4 | 0.062 | 5.7 | LOS A | 0.3 | 2.0 | 0.06 | 0.55 | 0.06 | 52.9 |
| 2 T1 | 69 | 0.0 | 73 | 0.0 | 0.116 | 4.7 | LOS A | 0.4 | 3.3 | 0.27 | 0.56 | 0.27 | 53.8 |
| 3 R2 | 40 | 30.0 | 42 | 30.0 | 0.116 | 7.2 | LOS A | 0.4 | 3.3 | 0.27 | 0.56 | 0.27 | 51.8 |
| Approach | 199 | 11.6 | 209 | 11.6 | 0.116 | 5.7 | LOS A | 0.4 | 3.3 | 0.17 | 0.56 | 0.17 | 53.0 |
| East: Commerial Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 42 | 16.7 | 44 | 16.7 | 0.040 | 5.7 | LOS A | 0.1 | 0.6 | 0.02 | 0.47 | 0.02 | 53.6 |
| 5 T1 | 11 | 15.4 | 12 | 15.4 | 0.040 | 0.0 | LOSA | 0.1 | 0.6 | 0.02 | 0.47 | 0.02 | 55.8 |
| 6 R2 | 8 | 25.0 | 8 | 25.0 | 0.040 | 5.8 | LOS A | 0.1 | 0.6 | 0.02 | 0.47 | 0.02 | 52.7 |
| Approach | 61 | 17.5 | 64 | 17.5 | 0.040 | 4.7 | NA | 0.1 | 0.6 | 0.02 | 0.47 | 0.02 | 53.9 |
| North: Bocks Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 2 | 0.0 | 2 | 0.0 | 0.052 | 5.6 | LOS A | 0.2 | 1.4 | 0.17 | 0.53 | 0.17 | 54.1 |
| 8 T1 | 51 | 5.9 | 54 | 5.9 | 0.052 | 4.9 | LOS A | 0.2 | 1.4 | 0.17 | 0.53 | 0.17 | 54.0 |
| 9 R2 | 2 | 0.0 | 2 | 0.0 | 0.052 | 6.9 | LOSA | 0.2 | 1.4 | 0.17 | 0.53 | 0.17 | 53.6 |
| Approach | 55 | 5.5 | 58 | 5.5 | 0.052 | 5.0 | LOS A | 0.2 | 1.4 | 0.17 | 0.53 | 0.17 | 54.0 |
| West: Commerial Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 5 | 0.0 | 5 | 0.0 | 0.068 | 5.8 | LOSA | 0.3 | 2.1 | 0.15 | 0.50 | 0.15 | 53.6 |
| 11 T1 | 8 | 0.0 | 8 | 0.0 | 0.068 | 0.2 | LOS A | 0.3 | 2.1 | 0.15 | 0.50 | 0.15 | 54.9 |
| 12 R 2 | 77 | 4.2 | 81 | 4.2 | 0.068 | 5.8 | LOSA | 0.3 | 2.1 | 0.15 | 0.50 | 0.15 | 53.1 |
| Approach | 90 | 3.6 | 95 | 3.6 | 0.068 | 5.3 | NA | 0.3 | 2.1 | 0.15 | 0.50 | 0.15 | 53.3 |
| All <br> Vehicles | 405 | 9.9 | 426 | 9.9 | 0.116 | 5.3 | NA | 0.4 | 3.3 | 0.15 | 0.53 | 0.15 | 53.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

$\nabla$ Site: 101 [PM Existing + Background Growth + Growth (High
Case) (Site Folder: General)]
New Site
Site Category: (None)
Give-Way (Two-Way)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{array}{r} \text { IN } \\ \text { VOL } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{aligned} & \text { UT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \end{aligned}$ | $\begin{aligned} & \text { DEM } \\ & \text { FLO } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{gathered} \text { AND } \\ \text { WS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn <br> v/c | Aver. Delay sec $\qquad$ | Level of Service | $\begin{gathered} \text { 95\% BA } \\ \text { QUE } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| South: Chapman Road (S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 97 | 12.4 | 102 | 12.4 | 0.067 | 5.7 | LOSA | 0.3 | 2.2 | 0.06 | 0.55 | 0.06 | 52.9 |
| 2 T1 | 69 | 0.0 | 73 | 0.0 | 0.119 | 4.8 | LOSA | 0.4 | 3.3 | 0.29 | 0.57 | 0.29 | 53.7 |
| 3 R2 | 40 | 30.0 | 42 | 30.0 | 0.119 | 7.3 | LOSA | 0.4 | 3.3 | 0.29 | 0.57 | 0.29 | 51.7 |
| Approach | 206 | 11.7 | 217 | 11.7 | 0.119 | 5.7 | LOS A | 0.4 | 3.3 | 0.18 | 0.56 | 0.18 | 52.9 |
| East: Commerial Road (E) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 L2 | 42 | 16.7 | 44 | 16.7 | 0.041 | 5.7 | LOSA | 0.1 | 0.6 | 0.02 | 0.45 | 0.02 | 53.8 |
| 5 T1 | 13 | 15.4 | 14 | 15.4 | 0.041 | 0.0 | LOSA | 0.1 | 0.6 | 0.02 | 0.45 | 0.02 | 55.9 |
| 6 R2 | 8 | 25.0 | 8 | 25.0 | 0.041 | 5.8 | LOS A | 0.1 | 0.6 | 0.02 | 0.45 | 0.02 | 52.8 |
| Approach | 63 | 17.5 | 66 | 17.5 | 0.041 | 4.6 | NA | 0.1 | 0.6 | 0.02 | 0.45 | 0.02 | 54.1 |
| North: Bocks Road (N) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 2 | 0.0 | 2 | 0.0 | 0.053 | 5.6 | LOSA | 0.2 | 1.4 | 0.17 | 0.54 | 0.17 | 54.0 |
| 8 T1 | 51 | 5.9 | 54 | 5.9 | 0.053 | 5.0 | LOS A | 0.2 | 1.4 | 0.17 | 0.54 | 0.17 | 54.0 |
| 9 R2 | 2 | 0.0 | 2 | 0.0 | 0.053 | 7.1 | LOSA | 0.2 | 1.4 | 0.17 | 0.54 | 0.17 | 53.5 |
| Approach | 55 | 5.5 | 58 | 5.5 | 0.053 | 5.1 | LOS A | 0.2 | 1.4 | 0.17 | 0.54 | 0.17 | 54.0 |
| West: Commerial Road (W) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 L2 | 5 | 0.0 | 5 | 0.0 | 0.083 | 5.8 | LOSA | 0.4 | 2.6 | 0.16 | 0.51 | 0.16 | 53.5 |
| 11 T1 | 8 | 0.0 | 8 | 0.0 | 0.083 | 0.2 | LOS A | 0.4 | 2.6 | 0.16 | 0.51 | 0.16 | 54.9 |
| 12 R 2 | 95 | 4.2 | 100 | 4.2 | 0.083 | 5.8 | LOS A | 0.4 | 2.6 | 0.16 | 0.51 | 0.16 | 53.1 |
| Approach | 108 | 3.7 | 114 | 3.7 | 0.083 | 5.4 | NA | 0.4 | 2.6 | 0.16 | 0.51 | 0.16 | 53.2 |
| All <br> Vehicles | 432 | 9.7 | 455 | 9.7 | 0.119 | 5.4 | NA | 0.4 | 3.3 | 0.15 | 0.53 | 0.15 | 53.3 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Minor Road Approach LOS values are based on average delay for all vehicle movements.
NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

Site: 101 [AM Existing (Site Folder: General)]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=140$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | $\begin{gathered} \text { JT } \\ \text { VES } \\ \text { HV ] } \\ \% \end{gathered}$ |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 126 | 7.4 | 126 | 7.4 | 0.100 | 7.4 | LOS A | 1.2 | 9.1 | 0.20 | 0.60 | 0.20 | 52.8 |
| 22 T1 | 1324 | 5.2 | 1324 | 5.2 | 0.657 | 18.9 | LOS B | 28.5 | 208.1 | 0.68 | 0.62 | 0.68 | 45.9 |
| 23 R2 | 93 | 8.5 | 93 | 8.5 | * 0.744 | 80.1 | LOS F | 6.7 | 50.5 | 1.00 | 0.85 | 1.17 | 25.6 |
| Approach | 1543 | 5.6 | 1543 | 5.6 | 0.744 | 21.6 | LOS B | 28.5 | 208.1 | 0.66 | 0.63 | 0.67 | 44.2 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 54 | 6.5 | 54 | 6.5 | 0.083 | 18.5 | LOS B | 1.6 | 11.6 | 0.49 | 0.67 | 0.49 | 45.5 |
| 25 T1 | 19 | 5.1 | 19 | 5.1 | 0.083 | 59.3 | LOSE | 1.2 | 8.5 | 0.92 | 0.66 | 0.92 | 30.5 |
| 26 R2 | 56 | 6.2 | 56 | 6.2 | 0.226 | 58.8 | LOSE | 3.4 | 25.0 | 0.90 | 0.73 | 0.90 | 30.3 |
| Approach | 129 | 6.2 | 129 | 6.2 | 0.226 | 42.0 | LOS C | 3.4 | 25.0 | 0.73 | 0.69 | 0.73 | 35.3 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 112 | 4.7 | 112 | 4.7 | 0.090 | 7.6 | LOS A | 1.2 | 8.8 | 0.21 | 0.60 | 0.21 | 52.6 |
| 28 T1 | 1655 | 4.9 | 1655 | 4.9 | * 0.786 | 21.8 | LOS B | 40.9 | 298.5 | 0.79 | 0.73 | 0.79 | 44.2 |
| 29 R2 | 67 | 4.1 | 67 | 4.1 | 0.520 | 76.4 | LOS F | 4.6 | 33.5 | 1.00 | 0.76 | 1.00 | 26.4 |
| Approach | 1834 | 4.9 | 1834 | 4.9 | 0.786 | 22.9 | LOS B | 40.9 | 298.5 | 0.76 | 0.72 | 0.76 | 43.6 |
| SouthWest: Chapman Road (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 78 | 4.7 | 78 | 4.7 | 0.100 | 12.9 | LOS A | 1.7 | 12.4 | 0.38 | 0.65 | 0.38 | 48.9 |
| 31 T1 | 25 | 4.4 | 25 | 4.4 | * 0.109 | 59.5 | LOS E | 1.5 | 11.2 | 0.92 | 0.67 | 0.92 | 30.5 |
| 32 R 2 | 67 | 6.9 | 67 | 6.9 | * 0.267 | 59.3 | LOS E | 4.1 | 30.3 | 0.91 | 0.74 | 0.91 | 30.1 |
| Approach | 170 | 5.5 | 170 | 5.5 | 0.267 | 38.1 | LOS C | 4.1 | 30.3 | 0.67 | 0.69 | 0.67 | 36.7 |
| All Vehicles | 3676 | 5.2 | 3676 | 5.2 | 0.786 | 23.7 | LOS B | 40.9 | 298.5 | 0.71 | 0.68 | 0.72 | 43.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{\text {ID }}^{\text {Mov }} \text { Crossing }$ | Input Vol. <br> ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of AVERAGE BACK OF Service QUEUE |  |  |  |  | Travel Time sec | Travel Dist. <br> m | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |
| P5 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 233.9 | 220.5 | 0.94 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |
| P6 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 229.8 | 215.2 | 0.94 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |
| P7 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 233.9 | 220.5 | 0.94 |

## MOVEMENT SUMMARY

Site: 101 [AM Existing + Growth (Site Folder: General)]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=150$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { INF } \\ \text { VOLU } \\ \text { [ Total } \\ \text { veh/h } \\ \hline \end{array}$ | $\begin{gathered} \text { JT } \\ \text { MES } \\ \text { HV ] } \\ \% \end{gathered}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service |  | $\begin{gathered} \text { CK OF } \\ \text { =UE } \\ \text { Dist ] } \\ \mathrm{m} \end{gathered}$ | Prop. Que | Effective Stop Rate |  | Aver Speed <br> km/h |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 151 | 7.4 | 151 | 7.4 | 0.121 | 7.7 | LOS A | 1.7 | 12.4 | 0.20 | 0.60 | 0.20 | 52.6 |
| 22 T1 | 1589 | 5.2 | 1589 | 5.2 | 0.784 | 21.1 | LOS B | 40.7 | 297.8 | 0.74 | 0.68 | 0.74 | 44.6 |
| 23 R2 | 112 | 8.5 | 112 | 8.5 | * 0.872 | 91.7 | LOS F | 9.1 | 68.6 | 1.00 | 0.96 | 1.40 | 23.7 |
| Approach | 1852 | 5.6 | 1852 | 5.6 | 0.872 | 24.3 | LOS B | 40.7 | 297.8 | 0.71 | 0.69 | 0.74 | 42.9 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 65 | 6.5 | 65 | 6.5 | 0.122 | 31.5 | LOS C | 2.8 | 20.9 | 0.65 | 0.71 | 0.65 | 39.2 |
| 25 T1 | 23 | 5.1 | 23 | 5.1 | 0.102 | 63.9 | LOS E | 1.5 | 11.0 | 0.92 | 0.67 | 0.92 | 29.4 |
| 26 R2 | 67 | 6.2 | 67 | 6.2 | 0.285 | 64.1 | LOS E | 4.4 | 32.6 | 0.92 | 0.74 | 0.92 | 29.0 |
| Approach | 155 | 6.2 | 155 | 6.2 | 0.285 | 50.4 | LOS D | 4.4 | 32.6 | 0.81 | 0.72 | 0.81 | 32.6 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 134 | 4.7 | 134 | 4.7 | 0.109 | 8.0 | LOS A | 1.7 | 12.3 | 0.22 | 0.61 | 0.22 | 52.3 |
| 28 T1 | 1986 | 4.9 | 1986 | 4.9 | * 0.937 | 46.2 | LOS D | 77.7 | 567.0 | 0.91 | 0.96 | 1.05 | 34.2 |
| 29 R2 | 80 | 4.1 | 80 | 4.1 | 0.605 | 81.7 | LOS F | 6.0 | 43.1 | 1.00 | 0.78 | 1.03 | 25.4 |
| Approach | 2200 | 4.9 | 2200 | 4.9 | 0.937 | 45.1 | LOS D | 77.7 | 567.0 | 0.87 | 0.93 | 1.00 | 34.5 |
| SouthWest: Chapman Road (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 94 | 4.7 | 94 | 4.7 | 0.139 | 18.2 | LOS B | 2.9 | 20.9 | 0.48 | 0.68 | 0.48 | 45.7 |
| 31 T1 | 30 | 4.4 | 30 | 4.4 | * 0.132 | 64.1 | LOS E | 2.0 | 14.4 | 0.93 | 0.68 | 0.93 | 29.4 |
| 32 R2 | 80 | 6.9 | 80 | 6.9 | * 0.335 | 64.7 | LOS E | 5.3 | 39.6 | 0.92 | 0.75 | 0.92 | 28.9 |
| Approach | 204 | 5.5 | 204 | 5.5 | 0.335 | 43.2 | LOS D | 5.3 | 39.6 | 0.72 | 0.71 | 0.72 | 34.9 |
| All Vehicles | 4411 | 5.2 | 4411 | 5.2 | 0.937 | 36.5 | LOS C | 77.7 | 567.0 | 0.79 | 0.81 | 0.87 | 37.5 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

Pedestrian Movement Performance

| Mov ID Crossing | Input Vol. ped/h | Dem. Flow ped/h | Aver. Delay <br> sec | Level of AVERAGE BACK OF Service QUEUE |  |  | Prop. Effective Que Stop Rate |  | Travel Time sec | Travel Dist. <br> m | Aver. <br> Speed <br> m/sec |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |
| P5 Full | 50 | 50 | 69.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 238.9 | 220.5 | 0.92 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |
| P6 Full | 50 | 50 | 69.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 234.8 | 215.2 | 0.92 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |

## MOVEMENT SUMMARY

## 目 Site: 101 [AM Existing + Growth + Proposal (Site Folder: <br> General)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=150$ seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{aligned} & \text { INF } \\ & \text { VOL } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{aligned} & \text { JT } \\ & \text { VES } \\ & \text { HV ] } \\ & \% \end{aligned}$ | $\begin{gathered} \text { DEM } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \end{gathered}$ | $\begin{gathered} \text { ND } \\ \text { VS } \\ \text { HV ] } \\ \% \end{gathered}$ | Deg. Satn $\qquad$ v/c | Aver. Delay $\qquad$ sec | Level of Service | 95\% B <br> QU <br> [ Veh. <br> veh | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate |  | Aver. Speed $\qquad$ km/h |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 151 | 7.4 | 151 | 7.4 | 0.121 | 7.7 | LOS A | 1.7 | 12.4 | 0.20 | 0.60 | 0.20 | 52.6 |
| 22 T1 | 1589 | 5.2 | 1589 | 5.2 | 0.788 | 21.1 | LOS B | 40.4 | 295.4 | 0.74 | 0.68 | 0.74 | 44.6 |
| 23 R2 | 124 | 8.5 | 124 | 8.5 | * 0.966 | 114.6 | LOS F | 11.7 | 87.6 | 1.00 | 1.13 | 1.78 | 20.7 |
| Approach | 1864 | 5.6 | 1864 | 5.6 | 0.966 | 26.3 | LOS B | 40.4 | 295.4 | 0.71 | 0.70 | 0.76 | 41.9 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 70 | 6.5 | 70 | 6.5 | 0.131 | 31.6 | LOS C | 3.1 | 22.6 | 0.65 | 0.71 | 0.65 | 39.2 |
| 25 T1 | 23 | 5.1 | 23 | 5.1 | 0.102 | 63.9 | LOS E | 1.5 | 11.0 | 0.92 | 0.67 | 0.92 | 29.4 |
| 26 R2 | 70 | 6.2 | 70 | 6.2 | 0.298 | 64.3 | LOS E | 4.6 | 34.1 | 0.93 | 0.74 | 0.93 | 29.0 |
| Approach | 163 | 6.2 | 163 | 6.2 | 0.298 | 50.2 | LOS D | 4.6 | 34.1 | 0.81 | 0.72 | 0.81 | 32.7 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 140 | 4.7 | 140 | 4.7 | 0.115 | 8.2 | LOS A | 1.9 | 13.5 | 0.23 | 0.61 | 0.23 | 52.2 |
| 28 T1 | 1986 | 4.9 | 1986 | 4.9 | * 0.939 | 47.1 | LOS D | 78.6 | 573.2 | 0.91 | 0.96 | 1.05 | 33.9 |
| 29 R2 | 80 | 4.1 | 80 | 4.1 | 0.605 | 81.7 | LOS F | 6.0 | 43.1 | 1.00 | 0.78 | 1.03 | 25.4 |
| Approach | 2206 | 4.9 | 2206 | 4.9 | 0.939 | 45.9 | LOS D | 78.6 | 573.2 | 0.87 | 0.93 | 1.00 | 34.3 |
| SouthWest: Chapman Road (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 94 | 4.7 | 94 | 4.7 | 0.140 | 18.2 | LOS B | 2.9 | 20.9 | 0.48 | 0.68 | 0.48 | 45.7 |
| 31 T1 | 30 | 4.4 | 30 | 4.4 | * 0.132 | 64.1 | LOS E | 2.0 | 14.4 | 0.93 | 0.68 | 0.93 | 29.4 |
| 32 R 2 | 80 | 6.9 | 80 | 6.9 | * 0.335 | 64.7 | LOS E | 5.3 | 39.6 | 0.92 | 0.75 | 0.92 | 28.9 |
| Approach | 204 | 5.5 | 204 | 5.5 | 0.335 | 43.2 | LOS D | 5.3 | 39.6 | 0.72 | 0.71 | 0.72 | 34.9 |
| All <br> Vehicles | 4437 | 5.2 | 4437 | 5.2 | 0.966 | 37.7 | LOS C | 78.6 | 573.2 | 0.79 | 0.82 | 0.88 | 37.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{\text {ID }} \begin{aligned} & \text { Mov } \\ & \text { Crossing } \end{aligned}$ | Input Vol. <br> ped/h | Dem. Flow <br> ped/h | Aver. Delay $\qquad$ | Level of Service |  | ACK OF E Dist ] $m$ | Prop. E Que | Effective Stop Rate | Travel Time $\qquad$ sec | Travel Dist. $\qquad$ | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |
| P5 Full | 50 | 50 | 69.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 238.9 | 220.5 | 0.92 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |
| P6 Full | 50 | 50 | 69.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 234.8 | 215.2 | 0.92 |

## MOVEMENT SUMMARY

## 目ite: 101 [AM Existing + Growth + Proposal (Low Case) (Site Folder: General)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 150 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { INP } \\ \text { VOLU } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{aligned} & \text { JT } \\ & \text { VES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn v/c | Aver. Delay sec | Level of Service | $\begin{gathered} \text { 95\% B B } \\ \text { Q } \\ \text { [ Veh. } \\ \text { veh } \end{gathered}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 151 | 7.4 | 151 | 7.4 | 0.121 | 7.7 | LOS A | 1.7 | 12.4 | 0.20 | 0.60 | 0.20 | 52.6 |
| 22 T1 | 1589 | 5.2 | 1589 | 5.2 | 0.786 | 21.1 | LOS B | 40.5 | 296.4 | 0.74 | 0.68 | 0.74 | 44.6 |
| 23 R2 | 119 | 8.5 | 119 | 8.5 | * 0.927 | 100.3 | LOS F | 10.3 | 77.4 | 1.00 | 1.05 | 1.60 | 22.5 |
| Approach | 1859 | 5.6 | 1859 | 5.6 | 0.927 | 25.1 | LOS B | 40.5 | 296.4 | 0.71 | 0.70 | 0.75 | 42.5 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 68 | 6.5 | 68 | 6.5 | 0.127 | 31.6 | LOS C | 3.0 | 21.9 | 0.65 | 0.71 | 0.65 | 39.2 |
| 25 T1 | 23 | 5.1 | 23 | 5.1 | 0.102 | 63.9 | LOS E | 1.5 | 11.0 | 0.92 | 0.67 | 0.92 | 29.4 |
| 26 R2 | 68 | 6.2 | 68 | 6.2 | 0.289 | 64.2 | LOS E | 4.5 | 33.1 | 0.92 | 0.74 | 0.92 | 29.0 |
| Approach | 159 | 6.2 | 159 | 6.2 | 0.289 | 50.2 | LOS D | 4.5 | 33.1 | 0.81 | 0.72 | 0.81 | 32.7 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 137 | 4.7 | 137 | 4.7 | 0.112 | 8.2 | LOS A | 1.8 | 13.1 | 0.23 | 0.61 | 0.23 | 52.2 |
| 28 T1 | 1986 | 4.9 | 1986 | 4.9 | * 0.937 | 46.1 | LOS D | 77.6 | 566.2 | 0.91 | 0.96 | 1.05 | 34.2 |
| 29 R2 | 80 | 4.1 | 80 | 4.1 | 0.605 | 81.7 | LOS F | 6.0 | 43.1 | 1.00 | 0.78 | 1.03 | 25.4 |
| Approach | 2203 | 4.9 | 2203 | 4.9 | 0.937 | 45.0 | LOS D | 77.6 | 566.2 | 0.87 | 0.93 | 0.99 | 34.5 |
| SouthWest: Chapman Road (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 94 | 4.7 | 94 | 4.7 | 0.140 | 18.2 | LOS B | 2.9 | 20.9 | 0.48 | 0.68 | 0.48 | 45.7 |
| 31 T1 | 30 | 4.4 | 30 | 4.4 | * 0.132 | 64.1 | LOS E | 2.0 | 14.4 | 0.93 | 0.68 | 0.93 | 29.4 |
| 32 R2 | 80 | 6.9 | 80 | 6.9 | * 0.335 | 64.7 | LOS E | 5.3 | 39.6 | 0.92 | 0.75 | 0.92 | 28.9 |
| Approach | 204 | 5.5 | 204 | 5.5 | 0.335 | 43.2 | LOS D | 5.3 | 39.6 | 0.72 | 0.71 | 0.72 | 34.9 |
| All <br> Vehicles | 4425 | 5.2 | 4425 | 5.2 | 0.937 | 36.7 | LOS C | 77.6 | 566.2 | 0.79 | 0.81 | 0.87 | 37.4 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & { }_{\text {ID }} \end{aligned}$ | Input Vol. <br> ped/h | Dem. Flow <br> ped/h | Aver. Delay $\qquad$ <br> sec | Level of Service |  | $\begin{aligned} & \text { ACK OF } \\ & \text { IE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate | Travel Time <br> sec | Travel Dist. $\qquad$ | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |
| P5 Full | 50 | 50 | 69.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 238.9 | 220.5 | 0.92 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |
| P6 Full | 50 | 50 | 69.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 234.8 | 215.2 | 0.92 |

## MOVEMENT SUMMARY

## 目ite: 101 [AM Existing + Growth + Proposal (High Case) (Site

Folder: General)]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 150 seconds (Site Optimum Cycle Time - Minimum Delay)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { IN } \\ \text { VOL } \\ \text { [ Total } \\ \text { veh/h } \end{array}$ | $\begin{gathered} \text { JT } \\ \text { VES } \\ \text { HV ] } \\ \% \end{gathered}$ | $\begin{gathered} \text { DEM } \\ \text { FLC } \\ \text { [ Total } \\ \text { veh/h } \\ \hline \end{gathered}$ | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay sec | Level of Service | 95\% B <br> QU <br> [ Veh. <br> veh | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> km/h |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 151 | 7.4 | 151 | 7.4 | 0.121 | 7.7 | LOS A | 1.7 | 12.4 | 0.20 | 0.60 | 0.20 | 52.6 |
| 22 T1 | 1589 | 5.2 | 1589 | 5.2 | 0.799 | 21.9 | LOS B | 41.0 | 299.7 | 0.75 | 0.69 | 0.75 | 44.2 |
| 23 R2 | 130 | 8.5 | 130 | 8.5 | * 0.928 | 100.3 | LOS F | 11.3 | 84.8 | 1.00 | 1.05 | 1.58 | 22.5 |
| Approach | 1870 | 5.6 | 1870 | 5.6 | 0.928 | 26.2 | LOS B | 41.0 | 299.7 | 0.72 | 0.71 | 0.76 | 41.9 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 73 | 6.5 | 73 | 6.5 | 0.136 | 32.9 | LOS C | 3.3 | 24.2 | 0.66 | 0.72 | 0.66 | 38.6 |
| 25 T1 | 23 | 5.1 | 23 | 5.1 | 0.102 | 63.9 | LOS E | 1.5 | 11.0 | 0.92 | 0.67 | 0.92 | 29.4 |
| 26 R2 | 71 | 6.2 | 71 | 6.2 | 0.302 | 64.3 | LOS E | 4.7 | 34.6 | 0.93 | 0.74 | 0.93 | 29.0 |
| Approach | 167 | 6.2 | 167 | 6.2 | 0.302 | 50.5 | LOS D | 4.7 | 34.6 | 0.81 | 0.72 | 0.81 | 32.6 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 143 | 4.7 | 143 | 4.7 | 0.118 | 8.4 | LOS A | 2.0 | 14.3 | 0.24 | 0.61 | 0.24 | 52.0 |
| 28 T1 | 1986 | 4.9 | 1986 | 4.9 | * 0.948 | 53.4 | LOS D | 83.2 | 606.5 | 0.92 | 1.01 | 1.10 | 32.0 |
| 29 R2 | 80 | 4.1 | 80 | 4.1 | 0.554 | 80.0 | LOS F | 5.9 | 42.5 | 1.00 | 0.77 | 1.00 | 25.7 |
| Approach | 2209 | 4.9 | 2209 | 4.9 | 0.948 | 51.5 | LOS D | 83.2 | 606.5 | 0.88 | 0.97 | 1.04 | 32.6 |
| SouthWest: Chapman Road (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 94 | 4.7 | 94 | 4.7 | 0.140 | 18.7 | LOS B | 2.9 | 21.3 | 0.49 | 0.68 | 0.49 | 45.4 |
| 31 T1 | 30 | 4.4 | 30 | 4.4 | * 0.132 | 64.1 | LOS E | 2.0 | 14.4 | 0.93 | 0.68 | 0.93 | 29.4 |
| 32 R2 | 80 | 6.9 | 80 | 6.9 | * 0.335 | 64.7 | LOS E | 5.3 | 39.6 | 0.92 | 0.75 | 0.92 | 28.9 |
| Approach | 204 | 5.5 | 204 | 5.5 | 0.335 | 43.4 | LOS D | 5.3 | 39.6 | 0.72 | 0.71 | 0.72 | 34.8 |
| All <br> Vehicles | 4450 | 5.3 | 4450 | 5.3 | 0.948 | 40.4 | LOS C | 83.2 | 606.5 | 0.80 | 0.84 | 0.90 | 36.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{\text {ID }} \begin{aligned} & \text { Mov } \\ & \text { Crossing } \end{aligned}$ | Input Vol. <br> ped/h | Dem. Flow <br> ped/h | Aver. Delay $\qquad$ <br> sec | Level of Service |  | $\begin{aligned} & \text { ACK OF } \\ & \text { IE } \\ & \text { Dist ] } \\ & \text { m } \end{aligned}$ | Prop. Que | Effective Stop Rate | Travel Time <br> sec | Travel Dist. $\qquad$ | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |
| P5 Full | 50 | 50 | 69.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 238.9 | 220.5 | 0.92 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |
| P6 Full | 50 | 50 | 69.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 234.8 | 215.2 | 0.92 |

## MOVEMENT SUMMARY

Site: 101 [PM Existing (Site Folder: General)]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=140$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { INP } \\ & \text { VOLU } \\ & \text { [ Total } \\ & \text { veh/h } \end{aligned}$ | $\begin{gathered} \text { JT } \\ \text { UES } \\ \text { HV ] } \\ \% \end{gathered}$ |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ | Level of Service |  | CK OF UE Dist] m | Prop. Que | Effective Stop Rate | Aver No. Cycles | Aver. Speed <br> km/h |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 97 | 6.4 | 97 | 6.4 | 0.077 | 7.4 | LOS A | 0.9 | 6.9 | 0.19 | 0.60 | 0.19 | 52.8 |
| 22 T1 | 1794 | 5.9 | 1794 | 5.9 | * 0.870 | 27.5 | LOS B | 51.4 | 378.3 | 0.85 | 0.81 | 0.88 | 41.4 |
| 23 R2 | 84 | 7.0 | 84 | 7.0 | * 0.831 | 85.3 | LOS F | 6.3 | 46.9 | 1.00 | 0.92 | 1.36 | 24.8 |
| Approach | 1975 | 6.0 | 1975 | 6.0 | 0.870 | 28.9 | LOS C | 51.4 | 378.3 | 0.82 | 0.81 | 0.87 | 40.7 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 79 | 6.0 | 79 | 6.0 | 0.097 | 11.3 | LOSA | 1.5 | 11.1 | 0.34 | 0.64 | 0.34 | 49.9 |
| 25 T1 | 31 | 7.2 | 31 | 7.2 | 0.137 | 60.0 | LOS E | 1.9 | 14.2 | 0.93 | 0.68 | 0.93 | 30.4 |
| 26 R2 | 61 | 6.9 | 61 | 6.9 | 0.230 | 56.2 | LOS D | 3.6 | 26.5 | 0.90 | 0.74 | 0.90 | 30.9 |
| Approach | 171 | 6.5 | 171 | 6.5 | 0.230 | 36.1 | LOS C | 3.6 | 26.5 | 0.65 | 0.68 | 0.65 | 37.4 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 97 | 4.0 | 97 | 4.0 | 0.078 | 7.6 | LOS A | 1.0 | 7.5 | 0.21 | 0.60 | 0.21 | 52.7 |
| 28 T1 | 1148 | 5.3 | 1148 | 5.3 | 0.514 | 17.6 | LOS B | 22.5 | 164.5 | 0.63 | 0.57 | 0.63 | 46.6 |
| 29 R2 | 59 | 4.9 | 59 | 4.9 | 0.575 | 79.3 | LOS F | 4.2 | 30.5 | 1.00 | 0.77 | 1.03 | 25.8 |
| Approach | 1304 | 5.2 | 1304 | 5.2 | 0.575 | 19.6 | LOS B | 22.5 | 164.5 | 0.62 | 0.58 | 0.62 | 45.3 |
| SouthWest: Chapman Road (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 86 | 5.0 | 86 | 5.0 | 0.140 | 23.1 | LOS B | 3.0 | 21.7 | 0.57 | 0.70 | 0.57 | 43.1 |
| 31 T1 | 33 | 5.2 | 33 | 5.2 | * 0.144 | 59.9 | LOS E | 2.0 | 14.9 | 0.93 | 0.69 | 0.93 | 30.4 |
| 32 R 2 | 84 | 6.3 | 84 | 6.3 | * 0.314 | 57.1 | LOS E | 5.0 | 36.9 | 0.92 | 0.75 | 0.92 | 30.7 |
| Approach | 203 | 5.6 | 203 | 5.6 | 0.314 | 43.1 | LOS D | 5.0 | 36.9 | 0.77 | 0.72 | 0.77 | 34.9 |
| All <br> Vehicles | 3653 | 5.7 | 3653 | 5.7 | 0.870 | 26.7 | LOS B | 51.4 | 378.3 | 0.74 | 0.72 | 0.76 | 41.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & { }_{\text {ID }} \end{aligned}$ | Input Vol. <br> ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of Service | AVERAC <br> [ Ped <br> ped | ACK OF E Dist ] | Prop. Que | Effective Stop Rate | Travel Time | Travel Dist. <br> m | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |
| P5 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 233.9 | 220.5 | 0.94 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |
| P6 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 229.8 | 215.2 | 0.94 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |
| P7 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 233.9 | 220.5 | 0.94 |

## MOVEMENT SUMMARY

Site: 101 [PM Existing + Growth (Site Folder: General)]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=140$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  |  |  | ND NS HV ] \% | Deg. Satn v/c | Aver. Delay <br> sec | Level of Service | 95\% <br> [ Veh. veh | CK OF UE Dist ] | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 116 | 6.4 | 116 | 6.4 | 0.093 | 7.6 | LOSA | 1.2 | 8.8 | 0.20 | 0.60 | 0.20 | 52.7 |
| 22 T1 | 2053 | 5.9 | 2053 | 5.9 | * 0.990 | 88.1 | LOS F | 103.4 | 760.8 | 0.96 | 1.25 | 1.40 | 24.6 |
| 23 R2 | 101 | 7.0 | 101 | 7.0 | * 0.888 | 89.0 | LOS F | 7.8 | 58.2 | 1.00 | 1.00 | 1.50 | 24.1 |
| Approach | 2270 | 6.0 | 2270 | 6.0 | 0.990 | 84.0 | LOS F | 103.4 | 760.8 | 0.93 | 1.20 | 1.34 | 25.3 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 95 | 6.0 | 95 | 6.0 | 0.134 | 14.4 | LOS A | 2.3 | 17.0 | 0.43 | 0.67 | 0.43 | 48.0 |
| 25 T1 | 37 | 7.2 | 37 | 7.2 | 0.164 | 60.3 | LOS E | 2.3 | 17.1 | 0.93 | 0.69 | 0.93 | 30.3 |
| 26 R2 | 73 | 6.9 | 73 | 6.9 | 0.310 | 59.6 | LOS E | 4.5 | 33.2 | 0.92 | 0.75 | 0.92 | 30.1 |
| Approach | 205 | 6.5 | 205 | 6.5 | 0.310 | 38.8 | LOS C | 4.5 | 33.2 | 0.70 | 0.70 | 0.70 | 36.4 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 116 | 4.0 | 116 | 4.0 | 0.094 | 8.0 | LOS A | 1.4 | 10.0 | 0.23 | 0.61 | 0.23 | 52.4 |
| 28 T1 | 1378 | 5.3 | 1378 | 5.3 | 0.645 | 18.6 | LOS B | 29.5 | 216.1 | 0.68 | 0.62 | 0.68 | 46.0 |
| 29 R2 | 71 | 4.9 | 71 | 4.9 | 0.615 | 78.6 | LOS F | 5.0 | 36.6 | 1.00 | 0.79 | 1.05 | 25.9 |
| Approach | 1565 | 5.2 | 1565 | 5.2 | 0.645 | 20.5 | LOS B | 29.5 | 216.1 | 0.66 | 0.63 | 0.67 | 44.8 |
| SouthWest: Chapman Road (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 103 | 5.0 | 103 | 5.0 | 0.195 | 34.8 | LOS C | 4.7 | 34.1 | 0.72 | 0.74 | 0.72 | 37.9 |
| 31 T1 | 40 | 5.2 | 40 | 5.2 | * 0.175 | 60.2 | LOS E | 2.5 | 18.2 | 0.93 | 0.70 | 0.93 | 30.3 |
| 32 R2 | 101 | 6.3 | 101 | 6.3 | * 0.424 | 61.5 | LOS E | 6.3 | 46.4 | 0.94 | 0.80 | 0.94 | 29.6 |
| Approach | 244 | 5.6 | 244 | 5.6 | 0.424 | 50.1 | LOS D | 6.3 | 46.4 | 0.85 | 0.75 | 0.85 | 32.8 |
| All <br> Vehicles | 4284 | 5.7 | 4284 | 5.7 | 0.990 | 56.7 | LOS E | 103.4 | 760.8 | 0.81 | 0.94 | 1.04 | 31.1 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & { }_{\text {ID }} \end{aligned}$ | Input Vol. <br> ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of Service | AVERAC <br> [ Ped <br> ped | ACK OF E Dist ] | Prop. Que | Effective Stop Rate | Travel Time | Travel Dist. <br> m | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |
| P5 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 233.9 | 220.5 | 0.94 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |
| P6 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 229.8 | 215.2 | 0.94 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |
| P7 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 233.9 | 220.5 | 0.94 |

## MOVEMENT SUMMARY

## 慁 Site: 101 [PM Existing + Growth + Proposal (Site Folder: <br> General)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=140$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID | $\begin{array}{r} \text { INF } \\ \text { VOLU } \\ \text { [ Total } \\ \text { veh/h } \\ \hline \end{array}$ | $\begin{gathered} \text { JT } \\ \text { VES } \\ \text { HV ] } \\ \% \end{gathered}$ |  | $\begin{aligned} & \text { IND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | $\begin{gathered} \text { 95\% BA } \\ \text { QUE } \\ \text { [ Veh. } \\ \text { veh } \\ \hline \end{gathered}$ | CK OF UE Dist ] m | Prop. Que | Effective Stop Rate |  | Aver. Speed <br> km/h |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 116 | 6.4 | 116 | 6.4 | 0.093 | 7.6 | LOS A | 1.2 | 8.8 | 0.20 | 0.60 | 0.20 | 52.7 |
| 22 T1 | 2053 | 5.9 | 2053 | 5.9 | * 0.992 | 90.0 | LOS F | 104.1 | 765.6 | 0.96 | 1.26 | 1.41 | 24.3 |
| 23 R2 | 107 | 7.0 | 107 | 7.0 | * 0.941 | 98.9 | LOS F | 8.9 | 66.0 | 1.00 | 1.09 | 1.72 | 22.7 |
| Approach | 2276 | 6.0 | 2276 | 6.0 | 0.992 | 86.3 | LOS F | 104.1 | 765.6 | 0.93 | 1.21 | 1.36 | 24.9 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 108 | 6.0 | 108 | 6.0 | 0.152 | 14.5 | LOS B | 2.7 | 19.6 | 0.44 | 0.67 | 0.44 | 47.9 |
| 25 T1 | 37 | 7.2 | 37 | 7.2 | 0.164 | 60.3 | LOS E | 2.3 | 17.1 | 0.93 | 0.69 | 0.93 | 30.3 |
| 26 R2 | 80 | 6.9 | 80 | 6.9 | 0.340 | 59.9 | LOS E | 4.9 | 36.6 | 0.93 | 0.75 | 0.93 | 30.0 |
| Approach | 225 | 6.5 | 225 | 6.5 | 0.340 | 38.2 | LOS C | 4.9 | 36.6 | 0.69 | 0.70 | 0.69 | 36.6 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 119 | 4.0 | 119 | 4.0 | 0.097 | 8.2 | LOS A | 1.5 | 10.8 | 0.23 | 0.61 | 0.23 | 52.2 |
| 28 T1 | 1378 | 5.3 | 1378 | 5.3 | 0.645 | 18.6 | LOS B | 29.5 | 215.9 | 0.68 | 0.62 | 0.68 | 46.0 |
| 29 R2 | 71 | 4.9 | 71 | 4.9 | 0.615 | 78.6 | LOS F | 5.0 | 36.6 | 1.00 | 0.79 | 1.05 | 25.9 |
| Approach | 1568 | 5.2 | 1568 | 5.2 | 0.645 | 20.5 | LOS B | 29.5 | 215.9 | 0.66 | 0.63 | 0.67 | 44.8 |
| SouthWest: Chapman Road (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 103 | 5.0 | 103 | 5.0 | 0.197 | 35.0 | LOS C | 4.7 | 34.2 | 0.72 | 0.74 | 0.72 | 37.8 |
| 31 T1 | 40 | 5.2 | 40 | 5.2 | * 0.175 | 60.2 | LOS E | 2.5 | 18.2 | 0.93 | 0.70 | 0.93 | 30.3 |
| 32 R2 | 101 | 6.3 | 101 | 6.3 | * 0.424 | 61.5 | LOS E | 6.3 | 46.4 | 0.94 | 0.80 | 0.94 | 29.6 |
| Approach | 244 | 5.6 | 244 | 5.6 | 0.424 | 50.1 | LOS D | 6.3 | 46.4 | 0.85 | 0.75 | 0.85 | 32.7 |
| All Vehicles | 4313 | 5.7 | 4313 | 5.7 | 0.992 | 57.8 | LOS E | 104.1 | 765.6 | 0.81 | 0.95 | 1.05 | 30.8 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{\text {ID }}^{\text {Mov }} \text { Crossing }$ | Input Vol. <br> ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of Service | VERAC <br> [Ped <br> ped | ACK OF <br> Dist ] | Prop. Que | Effective Stop Rate | Travel Time | Travel Dist. | Aver. Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |
| P5 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 233.9 | 220.5 | 0.94 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |
| P6 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 229.8 | 215.2 | 0.94 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |

## MOVEMENT SUMMARY

## Site: 101 [PM Existing + Growth + Proposal (Low Case) (Site <br> Folder: General)]

New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=140$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. <br> Satn <br> v/c | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed km/h |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 116 | 6.4 | 116 | 6.4 | 0.093 | 7.6 | LOS A | 1.2 | 8.8 | 0.20 | 0.60 | 0.20 | 52.7 |
| 22 T1 | 2053 | 5.9 | 2053 | 5.9 | * 0.991 | 89.1 | LOS F | 103.8 | 763.2 | 0.96 | 1.25 | 1.40 | 24.4 |
| 23 R2 | 104 | 7.0 | 104 | 7.0 | * 0.915 | 92.8 | LOS F | 8.3 | 61.6 | 1.00 | 1.04 | 1.60 | 23.6 |
| Approach | 2273 | 6.0 | 2273 | 6.0 | 0.991 | 85.1 | LOS F | 103.8 | 763.2 | 0.93 | 1.21 | 1.35 | 25.1 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 102 | 6.0 | 102 | 6.0 | 0.144 | 14.5 | LOS A | 2.5 | 18.4 | 0.43 | 0.67 | 0.43 | 47.9 |
| 25 T1 | 37 | 7.2 | 37 | 7.2 | 0.164 | 60.3 | LOS E | 2.3 | 17.1 | 0.93 | 0.69 | 0.93 | 30.3 |
| 26 R2 | 77 | 6.9 | 77 | 6.9 | 0.327 | 59.8 | LOS E | 4.7 | 35.1 | 0.93 | 0.75 | 0.93 | 30.0 |
| Approach | 216 | 6.5 | 216 | 6.5 | 0.327 | 38.5 | LOS C | 4.7 | 35.1 | 0.69 | 0.70 | 0.69 | 36.5 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 118 | 4.0 | 118 | 4.0 | 0.096 | 8.0 | LOS A | 1.4 | 10.2 | 0.23 | 0.61 | 0.23 | 52.4 |
| 28 T1 | 1378 | 5.3 | 1378 | 5.3 | 0.645 | 18.6 | LOS B | 29.5 | 216.0 | 0.68 | 0.62 | 0.68 | 46.0 |
| 29 R2 | 71 | 4.9 | 71 | 4.9 | 0.615 | 78.6 | LOS F | 5.0 | 36.6 | 1.00 | 0.79 | 1.05 | 25.9 |
| Approach | 1567 | 5.2 | 1567 | 5.2 | 0.645 | 20.5 | LOS B | 29.5 | 216.0 | 0.66 | 0.63 | 0.67 | 44.8 |
| SouthWest: Chapman Road (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 103 | 5.0 | 103 | 5.0 | 0.196 | 34.9 | LOS C | 4.7 | 34.2 | 0.72 | 0.74 | 0.72 | 37.9 |
| 31 T1 | 40 | 5.2 | 40 | 5.2 | * 0.175 | 60.2 | LOS E | 2.5 | 18.2 | 0.93 | 0.70 | 0.93 | 30.3 |
| 32 R2 | 101 | 6.3 | 101 | 6.3 | * 0.424 | 61.5 | LOS E | 6.3 | 46.4 | 0.94 | 0.80 | 0.94 | 29.6 |
| Approach | 244 | 5.6 | 244 | 5.6 | 0.424 | 50.1 | LOS D | 6.3 | 46.4 | 0.85 | 0.75 | 0.85 | 32.7 |
| All <br> Vehicles | 4300 | 5.7 | 4300 | 5.7 | 0.991 | 57.2 | LOS E | 103.8 | 763.2 | 0.81 | 0.95 | 1.04 | 30.9 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID Crossing | Input Vol. ped/h | Dem. Flow ped/h | Aver. Delay sec | Level of Service |  | $\begin{aligned} & \text { ACK OF } \\ & \text { E } \\ & \text { Dist ] } \\ & \mathrm{m} \end{aligned}$ | Prop. Que | fective <br> Stop <br> Rate | Travel Time sec | Travel Dist. m | Aver. Speed |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |
| P5 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 233.9 | 220.5 | 0.94 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |
| P6 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 229.8 | 215.2 | 0.94 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |

## MOVEMENT SUMMARY

## Site: 101 [PM Existing + Growth + Proposal (High Case) (Site

Folder: General)]
New Site
Site Category: (None)
Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time $=140$ seconds (Site User-Given Cycle Time)

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov Turn ID |  | $\begin{aligned} & \text { JT } \\ & \text { WES } \\ & \text { HV ] } \\ & \% \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay $\qquad$ | Level of Service | 95\% B QU [ Veh. veh | $\begin{aligned} & \text { CK OF } \\ & \text { EUE } \\ & \text { Dist ] } \\ & \mathrm{m} \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver No. Cycles | Aver. <br> Speed <br> $\mathrm{km} / \mathrm{h}$ |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 L2 | 116 | 6.4 | 116 | 6.4 | 0.093 | 7.6 | LOS A | 1.2 | 8.8 | 0.20 | 0.60 | 0.20 | 52.7 |
| 22 T1 | 2053 | 5.9 | 2053 | 5.9 | * 0.992 | 90.7 | LOS F | 104.3 | 767.2 | 0.96 | 1.26 | 1.41 | 24.2 |
| 23 R2 | 109 | 7.0 | 109 | 7.0 | * 0.959 | 105.2 | LOS F | 9.4 | 69.9 | 1.00 | 1.13 | 1.81 | 21.8 |
| Approach | 2278 | 6.0 | 2278 | 6.0 | 0.992 | 87.2 | LOS F | 104.3 | 767.2 | 0.93 | 1.22 | 1.37 | 24.7 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 L2 | 114 | 6.0 | 114 | 6.0 | 0.161 | 14.6 | LOS B | 2.8 | 20.9 | 0.44 | 0.67 | 0.44 | 47.8 |
| 25 T1 | 37 | 7.2 | 37 | 7.2 | 0.164 | 60.3 | LOS E | 2.3 | 17.1 | 0.93 | 0.69 | 0.93 | 30.3 |
| 26 R2 | 83 | 6.9 | 83 | 6.9 | 0.353 | 60.0 | LOSE | 5.1 | 38.1 | 0.93 | 0.75 | 0.93 | 30.0 |
| Approach | 234 | 6.5 | 234 | 6.5 | 0.353 | 37.9 | LOS C | 5.1 | 38.1 | 0.69 | 0.70 | 0.69 | 36.7 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 27 L2 | 120 | 4.0 | 120 | 4.0 | 0.098 | 8.2 | LOS A | 1.5 | 10.9 | 0.23 | 0.61 | 0.23 | 52.2 |
| 28 T1 | 1378 | 5.3 | 1378 | 5.3 | 0.645 | 18.6 | LOS B | 29.5 | 215.9 | 0.68 | 0.62 | 0.68 | 46.0 |
| 29 R2 | 71 | 4.9 | 71 | 4.9 | 0.615 | 78.6 | LOS F | 5.0 | 36.6 | 1.00 | 0.79 | 1.05 | 25.9 |
| Approach | 1569 | 5.2 | 1569 | 5.2 | 0.645 | 20.5 | LOS B | 29.5 | 215.9 | 0.66 | 0.63 | 0.67 | 44.8 |
| SouthWest: Chapman Road (SW) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30 L2 | 103 | 5.0 | 103 | 5.0 | 0.198 | 35.0 | LOS C | 4.7 | 34.3 | 0.72 | 0.74 | 0.72 | 37.8 |
| 31 T1 | 40 | 5.2 | 40 | 5.2 | * 0.175 | 60.2 | LOS E | 2.5 | 18.2 | 0.93 | 0.70 | 0.93 | 30.3 |
| 32 R2 | 101 | 6.3 | 101 | 6.3 | * 0.424 | 61.5 | LOS E | 6.3 | 46.4 | 0.94 | 0.80 | 0.94 | 29.6 |
| Approach | 244 | 5.6 | 244 | 5.6 | 0.424 | 50.1 | LOS D | 6.3 | 46.4 | 0.85 | 0.75 | 0.85 | 32.7 |
| All Vehicles | 4325 | 5.7 | 4325 | 5.7 | 0.992 | 58.2 | LOS E | 104.3 | 767.2 | 0.81 | 0.95 | 1.05 | 30.7 |

Site Level of Service (LOS) Method: Delay (RTA NSW). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Delay Model: SIDRA Standard (Geometric Delay is included).
Queue Model: SIDRA Standard.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

* Critical Movement (Signal Timing)

| Pedestrian Movement Performance |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{\text {ID }}^{\text {Mov }} \text { Crossing }$ | Input Vol. <br> ped/h | Dem. Flow ped/h | Aver. Delay <br> sec | Level of AVERAGE BACK OF Service QUEUE |  |  | Prop. EffectiveQueStop <br> Rate |  | Travel Time | Travel Dist. <br> m | Aver. <br> Speed <br> $\mathrm{m} / \mathrm{sec}$ |
| SouthEast: Windsor Road (SE) |  |  |  |  |  |  |  |  |  |  |  |
| P5 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 233.9 | 220.5 | 0.94 |
| NorthEast: Chapman Road (NE) |  |  |  |  |  |  |  |  |  |  |  |
| P6 Full | 50 | 50 | 64.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 | 229.8 | 215.2 | 0.94 |
| NorthWest: Windsor Road (NW) |  |  |  |  |  |  |  |  |  |  |  |

